

# **EINSTEIN TELESCOPE**

# Preliminary technical prefeasibility assessment based on Aubel's borehole results

**XIV ET Symposium | Maastricht** 

**ENGINEERING SERVICES BY TRACTEBEL ENGINEERING & AMBERG ENGINEERING** 





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# **Ground interpretation results from borehole Aubel Borehole Aubel : Stratigraphy and tectonics**



- Aubel borehole is in Paleozoic basement → the Famennian sandstone series
- This sandstone tectonic sheet outcrops on the hanging wall of a main trust to the west of the site.
- At the site scale, there is lack of structural data → Geological, structural conditions and, consequently, the rock mass characteristics are poorly defined





# Ground interpretation results from borehole Aubel **Borehole Aubel :** *Lithostratigraphy*

Eight lithological facies were recognized :

- The first four lithological facies correspond to medium-coarse grained sandstones:
  - GH: Homogenous sandstone
  - GL: Laminated sandstone
  - Gi: Heterogeneous sandstone with clayey component in the rock matrix (black spots, clayey pebbles...)
  - GHC: sandstone with calcareous component (HCI reaction)
  - A particular sandstone facies (HGH) is identified corresponding to a hydrothermal alteration of sandstones with a greenish aspect
- Two darker fine-grained materials are observed with siltstone (Slt) and clavev 2. level with calcareous component (ARG)
- A fault breccia facies at 2 levels: 152 and 164 m 3.



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Namurian

Famennian

Breccia

Visean

Lithology



# Ground interpretation results from borehole Aubel Aubel Borehole: *Joints identification*

A) Structural data between 150m to 170m (with and above the N-S fault zone)



Two structural domains were identified separated by the N-S Fault zone :

1. The structural domain above the N-S Fault zone is composed of:

- three sets of fractures/joints (Jn1, Jn2, Jn3) with a dip angle varying between 38 to 72°

- One fault orientation (Fault: N09-70E)
- two subsets representing the stratigraphical variation approaching fault-drag fault structure (S1a : N126-30SW and S1b : N185-60SW)
- 2. The structural domain below the N-S Fault zone is characterized by:
  - Four fracture sets (Jn2, Jn4, Jn5 and Jn6) with a dip angle from 56 to 83° (subvertical joints)
  - One fracture set associated to the fault (Jn-Fault)

- One well-constrained set corresponding to the stratification (S1c: N28- 24SE) with a dip angle varying between 20 to 41° (subhorizontal)





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## **Ground interpretation results from borehole Aubel Evaluation results**





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# **Ground interpretation results from borehole Aubel Evaluation results**



		Eq.	Q-		
Project Element	ESR	dimension system		Support requirements for vault	
		(m)	range		
Tunnel	0.8	10	10-66	Shotcrete thickness 5-6 cm + systematic bolting	
Shaft	0.8	15	0.04 -98	Range from RRS II to spot bolting	
Revision tunnel, Cavern F, G	1	12	10-67	Shotcrete thickness 5-6 cm + systematic bolting	
Dewatering/					
construction				Shoterata thickness 5-6 cm +	
tunnel &	1	6	10-67	suctomatic holting	
connection				systematic bolling	
tunnel BA					
Connection	1	8	10-67	Shotcrete thickness 5-6 cm +	
tunnel BC	I	0	10-07	systematic bolting	
Access tunnel	1.3	8	0.04 -98	Range from RRS I to no support	
Cavern A, Cx, D & G	0.8	38	2-96	Shotcrete thickness 9-12 cm +Bolts spaced by 2.1 m	
Cavern B	0.8	31	10-66	Shotcrete thickness 6-9 cm + Bolts spaced by 2.5 m	
Cavern Cy	0.8	21	10-66	Shotcrete thickness 5-6 cm + systematic bolting	
Cavern E	0.8	25	10-66	Shotcrete thickness 6-9 cm + Bolts spaced by 2.5 m	





# Subsurface conditions assessment for Aubel

#### **Reference layout feasibility assessment based on borehole data – Caverns**

Cavern (span> 20m) (only conventional method considered)				
From depth 200 to 250 m: high values of RQD (77-98%), excavation of the caverns is possible				
or cavern depth: Fresh rock				
Conventional method: possible in this zone with bolting and immediate support				
For cavern depth between 220 and 250 m: no broken core				
<ul> <li>✓ Conventional methods are possible</li> </ul>				
No fault zone from 220 to 250 m:				
Safe enverne exercision by conventional method				
Covern support & lining can be entimized, partial executation (i.e., NATM) is possible				
Dip angle changes from 20° to 84° along the depth				
Bolting and immediate lateral support. Might need face support				
Very high resistance rock mass, cavern support & lining can be optimised, partial excavation (i.e., NATM) is possible.				
<ul> <li>Concrete lining immediately following the excavation of front</li> </ul>				
✓ Shotcrete at the tunnel face				
The rock mass is strong (R4) to very strong (R5) drill and blast should be used				
Inknown water conditions at the depth of the caverns				
Monitoring water levels				
Pre-excavation probing				
Pregrouting might be required.				
IT water inflow is confirmed, might also need post excavation grouting.				





#### Subsurface conditions assessment for Aubel Reference layout feasibility assessment based on borehole data – Shafts

	Shaft				
RQD	Missing values of RQD for the first 150. From 150 to 250m, 94% of the borehole length has an RQD higher than 67%.				
	✓ Methods like SBC or drilling jumbos could be used				
	<ul> <li>Concrete lining to be installed immediately following the excavation for the fault zones</li> </ul>				
	✓ Lining of circular shaft could be optimised				
Weathering/	resh to slightly weathered rock from 150- 250m				
	✓ Methods like SBC seem safer as no data is available for the first 150 m				
alteration	Conventional methods are possible when combined with hard rock excavating methods (eg. drilling jumbo)				
Fault	2 Faults zones were identified: between 151 and 153 m and the second between 164 to 170 m with an alteration zone from 170-183 m				
Breccia/Gauge	<ul> <li>Methods like SBC are more appropriate</li> </ul>				
	<ul> <li>Concrete lining immediately following the excavation in these zones</li> </ul>				
Dip	Dip angle changes from 20° to 84° along the depth with steep dip angle encountered: possible flocking, lateral support needed				
	✓ Methods like SBC appear to be safer				
	<ul> <li>Concrete lining immediately following the excavation</li> </ul>				
UCS tests	✓ The use of gripper support is possible				
	<ul> <li>Lining of circular shaft could be optimised</li> </ul>				
	The use of conventional method like Drill and Blast might apply				
Strength index	✓ Drill and blast				
	✓ Unknown rock strength for the first 150 m, excavation method could not be generalized along the whole depth of the shaft				
Graphite	✓ Methods like SBC might be safer				
	<ul> <li>Concrete lining immediately following the excavation</li> </ul>				
Water	Unknown, the water table is at 9m below ground level which might imply the need of:				
conditions	Monitoring water levels				
	Draining pipes through final lining				
	<ul> <li>Permanent pumping</li> </ul>				
	Solution of the second seco				
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# Subsurface conditions assessment for Aubel

#### **Reference layout feasibility assessment based on borehole data – Tunnels**

	Tunnel and access/connection galleries (TBM and conventional method considered)				
RQD	For tunnel depth: high values of RQD (78-89%)				
	<ul> <li>Open TBM or gripper TBM is adequate for tunnel's depth (estimated below 200 m)</li> </ul>				
	<ul> <li>✓ Conventional method possible in this zone</li> </ul>				
Weathering/	For tunnel depth: Fresh rock				
alteration	✓ Open TBM is possible				
	✓ Drill and blast for connecting or auxiliary galleries of non-conventional diameter might be considered.				
Fault	At the depth of the tunnel, no fault zone were identified :				
Breccia/Gauge	<ul> <li>For tunnel depth: open TBM is possible, no notable uncemented faults</li> </ul>				
	<ul> <li>Conventional method : possible in this zone</li> </ul>				
	✓ Lining could be optimized				
Dip	Dip angle changes from 20° to 84° along the depth. Below 200 m, 4 families of joints identified and 1 bedding plane				
	Conser TDM essecibles helting and chatemate laws a suggest to an even stability of an all blocks				
	Open TBM possible, boiting and shotcrete layer support to ensure stability of small blocks				
	Conventional method: Support by bolting and shotcrete layer . Might need face support				
UCS tests	In the depth of the tunnel: Extremely high resistance rock mass, tunnel support & lining can be optimised				
	I ne use of gripper tunnel is possible				
	Mechanical method as roadheader might not be suitable				
Strength Index	I he rock mass is strong (R4) to very strong (R5), drill and blast should be used.				
Graphite	<ul> <li>Concrete lining immediately following the excavation of front</li> </ul>				
	✓ Shotcrete at the tunnel face				
Water conditions	Unknown water conditions at the depth of the tunnel				
	✓ Monitoring water levels				
	✓ Pre-excavation probing				
	<ul> <li>Pregrouting might be required.</li> </ul>				
	Permanent pump sumps required, if the layout cannot be modified with inclined tunnels				
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#### Subsurface conditions assessment for Aubel Reference layout feasibility assessment – Conclusions

Confronting the ground conditions to the construction elements	Cavern (span> 20m) (only conventional method considered)	Tunnel and access/connection galleries (TBM and conventional method considered)	Shaft
Conclusion: considering the most exclusive criteria	<ul> <li>Conventional methods could be used along with a support system of shotcrete and systematic bolting</li> <li>Drill and blast is suitable</li> </ul>	<ul> <li>Open TBM</li> <li>Conventional method with shotcrete layer and systematic bolting</li> </ul>	<ul> <li>No data for the whole depth of the shaft</li> <li>Methods like SBC could be more appropriate</li> </ul>
		<ul> <li>Avoid profusion of water when excavating</li> </ul>	<ul> <li>Avoid profusion of water when excavating in case clay exists</li> <li>Concrete lining immediately following the excavation in the fault zones</li> </ul>





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## **Questions round**

Thank you for your attention

