Cryogenic suspension with flexures in compression

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- Introduction: concept and hardware description.
- Mechanical behaviour.
- Heat extraction performance.
- Displacement thermal noise.
- Conclusions and future work.

Introduction

Requirements and features:

- Allow the extraction of 0.5 W in heat.
- Soft for low displacement thermal noise: pendulum mode at 356 mHz.
- Mechanically robust: safety factor of 6 in compression.
- Damp the internal resonances with an active control system.
- Optical anti-spring to lower the pendulum resonance frequency.



Key element: a short and thin flexure

 Its geometry is suitable for heat extraction: thin but short.





• It's a spring that can be made soft:

- It's robust because it works under the compression of the load: compressive strength of silicon is 3200 MPa at room temperature.
- For lower thermal noise, it is likely easier to achieve a good surface quality in a small flexure than in a long suspension rod.



Side view

Front cross section view

Mirror side 3D-CAD



Based on Joris' presentation last year



Hardware configuration

- Active control system from the Intermediate Mass:
 - Mirror general control.
 - Damping the pendulum and unwanted resonant modes.
 - A recoil mass around the mirror is not needed.
- Optical anti-spring to lower the resonance frequency.
- Joints with Gallium brazing: it can be disassembled.
- The counterweights are useful to modify mechanical behaviour.
- Leonardo will talk about the spring blades.



What we analyzed

- We present results for 1 particular flexure out of 9 analyzed.
- Displacement transfer functions, suspension thermal noise: one pendulum 1 × suspension beam, 2 × flexures, load of 50 kg.
- Heat extraction: cryogenic payload
- Material strength in compression: 3200 MPa.
- The safety factor in tension is \sim 50.

- Buckling: we checked that none of the resonant mode frequencies goes to zero.
- We compared with a suspension rod *whose ends have not been engineered*:
 - Safety factor 6 and 2 metres.
 - Material strength in tension: 120 MPa.



At the thinnest part, the safety factor is \sim 50.

Mechanical behaviour

- Displacement transfer functions
- Silicon anisotropic stiffness matrix.
- Direction [100] pointing upwards for all components.
- Bulk loss angle: $\phi = 1 \times 10^{-9}$.
- We used Ansys and COMSOL.



Displacement transfer functions (3)



• The rods are better between 20 and 35 Hz by 65 times and above 40 Hz by 50 times.

Displacement transfer functions: counterweight



Transverse transfer function





Fixed at 4 K 0.125 W heat source • Assembly initial temperature: 4 K. • Symmetric boundary conditions.

Displacement thermal noise

- Admittance transfer function: $A = \frac{V}{F}$
 - *V*: velocity
 - *F*: force
- Bulk loss angle: $\phi = 1 \times 10^{-9}$ (constant in temperature).
- Temperature is assumed to be uniform.
- The average temperature was used.



Displacement thermal noise



30 and 50 Hz: \sim 8.8 and 4.3 times respectively.

Future work

- Analysis of an optical anti-spring to lower the pendulum resonance frequency.
- Cooling time from room temperature (including movable cold fingers).
- Complete the design of the mechanical design of the payload.
- Consider small flexures made of ²⁸Si: its thermal conductivity is ten times larger.
- Spring blade design.
- Consider different Si crystal orientations for components.
- Consider contributions to the loss angle other than the bulk's.
- Calculate requirements for sensors and actuators.
- Design a prototype

Conclusions

- Flexures are robust and soft components with good heat extraction qualities.
- The system would be easy to assemble and disassemble.
- Their use requires using suspension beams with internal resonances that must be damped.
- The configuration allows the implementation of an active control system.
- A recoil mass around the test mass mirror is not necessary.
- We likely require a two-level payload to achieve the required displacement thermal noise.