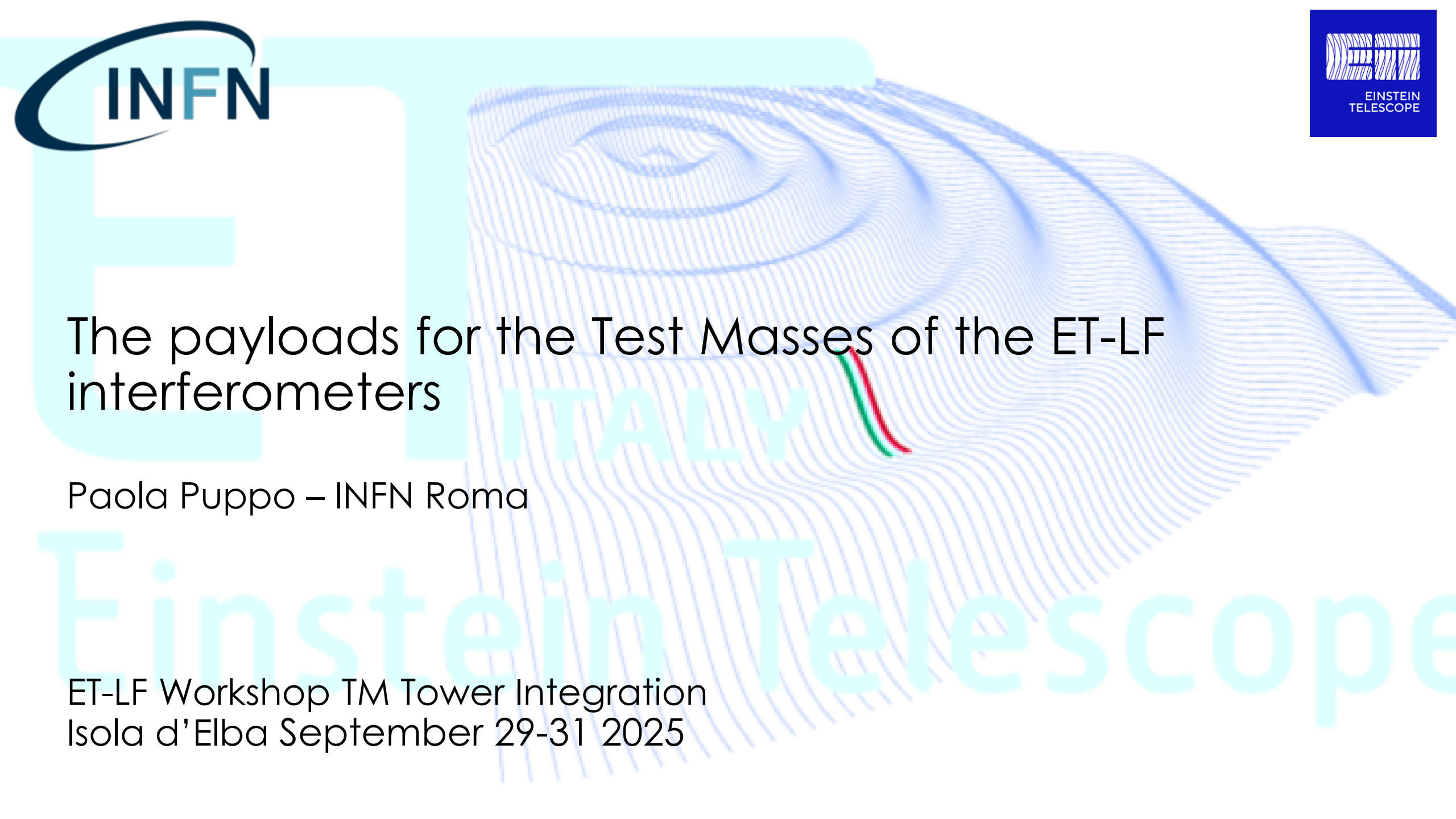




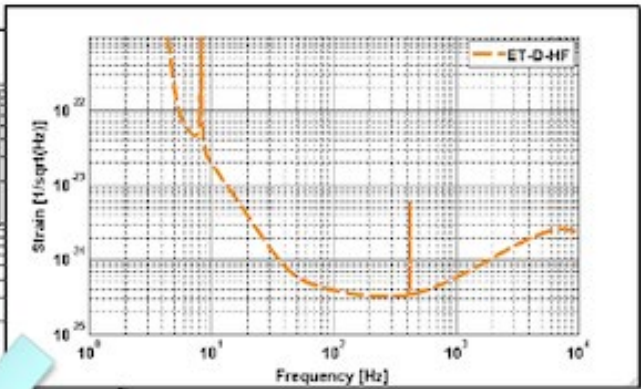
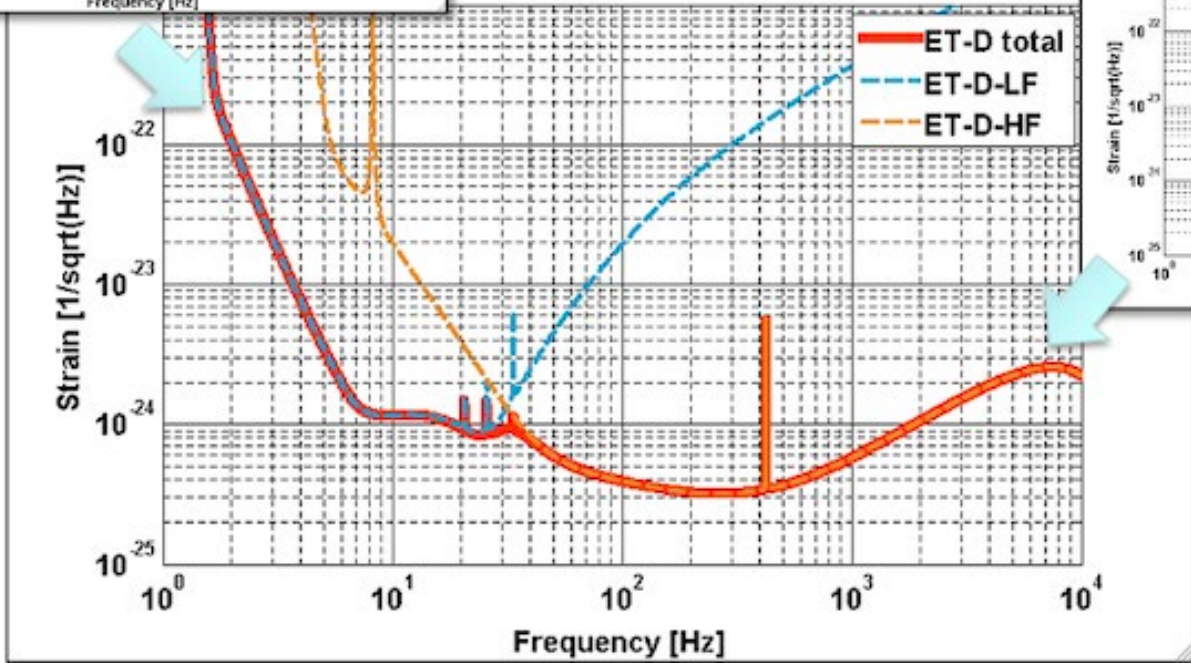
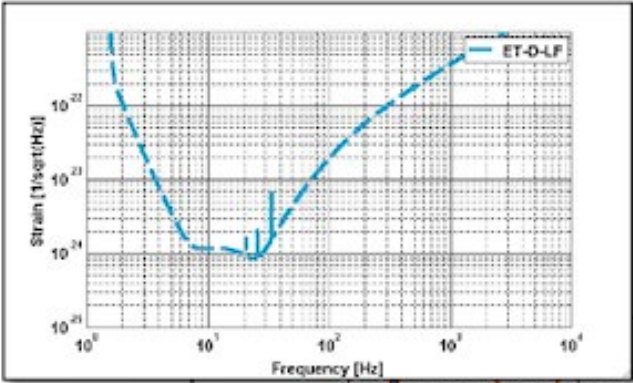
The payloads for the Test Masses of the ET-LF interferometers

Paola Puppo – INFN Roma

ET-LF Workshop TM Tower Integration
Isola d'Elba September 29-31 2025

Einstein Telescope is a hybrid detector composed of LF + HF interferometers

From Design Report Update 2020: ET-0007B-20



Parameter	ET-LF
Arm length	10 km
Input power (after IMC)	3 W
Arm power	18 kW
Temperature	10-20 K
Mirror material	silicon
Mirror diameter / thickness	45 cm/ 57 cm
Mirror masses	211 kg
Laser wavelength	1550 nm
SR-phase (rad)	detuned (0.6)
SR transmittance	20 %
Quantum noise suppression	freq. dep. squeeze.
Filter cavities	2x1.0 km
Squeezing level	10 dB (effective)
Beam shape	TEM ₀₀
Beam radius	9 cm
Scatter loss per surface	37 ppm
Seismic isolation	mod SA, 17 m tall
Seismic (for $f > 1$ Hz)	$5 \cdot 10^{-10} \text{ m}/f^2$
Gravity gradient subtraction	factor of a few

Parameter	ET-HF
Arm length	10 km
Input power (after IMC)	500 W
Arm power	3 MW
Temperature	290 K
Mirror material	fused silica
Mirror diameter / thickness	62 cm / 30 cm
Mirror masses	200 kg
Laser wavelength	1064 nm
SR-phase (rad)	tuned (0.0)
SR transmittance	10 %
Quantum noise suppression	freq. dep. squeeze.
Filter cavities	1x300 m
Squeezing level	10 dB (effective)
Beam shape	TEM ₀₀
Beam radius	12.0 cm
Scatter loss per surface	37 ppm
Seismic isolation	SA, 8 m tall
Seismic (for $f > 1$ Hz)	$5 \cdot 10^{-10} \text{ m}/f^2$
Gravity gradient subtraction	none



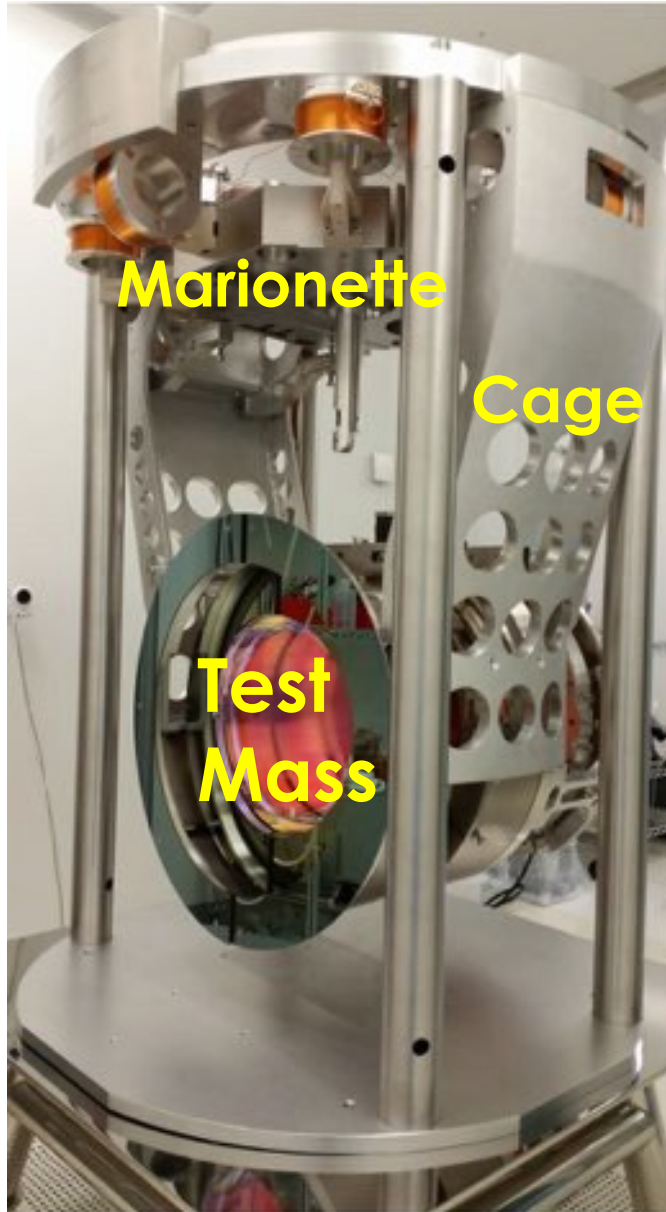
The Last Stage Suspension

The **role** of the Last Stage Suspension is

- to compensate the residual seismic noise
- to steer the optical components maintaining the relative position of the interferometer mirrors.

Bernardini A., Majorana E., Puppo P., Rapagnani P., Ricci F., Testi G. "Suspension last stages for the mirrors of the Virgo interferometric gravitational wave antenna." *Rev. Sci. Instr.* 70, no. 8 (1999): 3463.

Attached to the Last Filter of the upper suspension



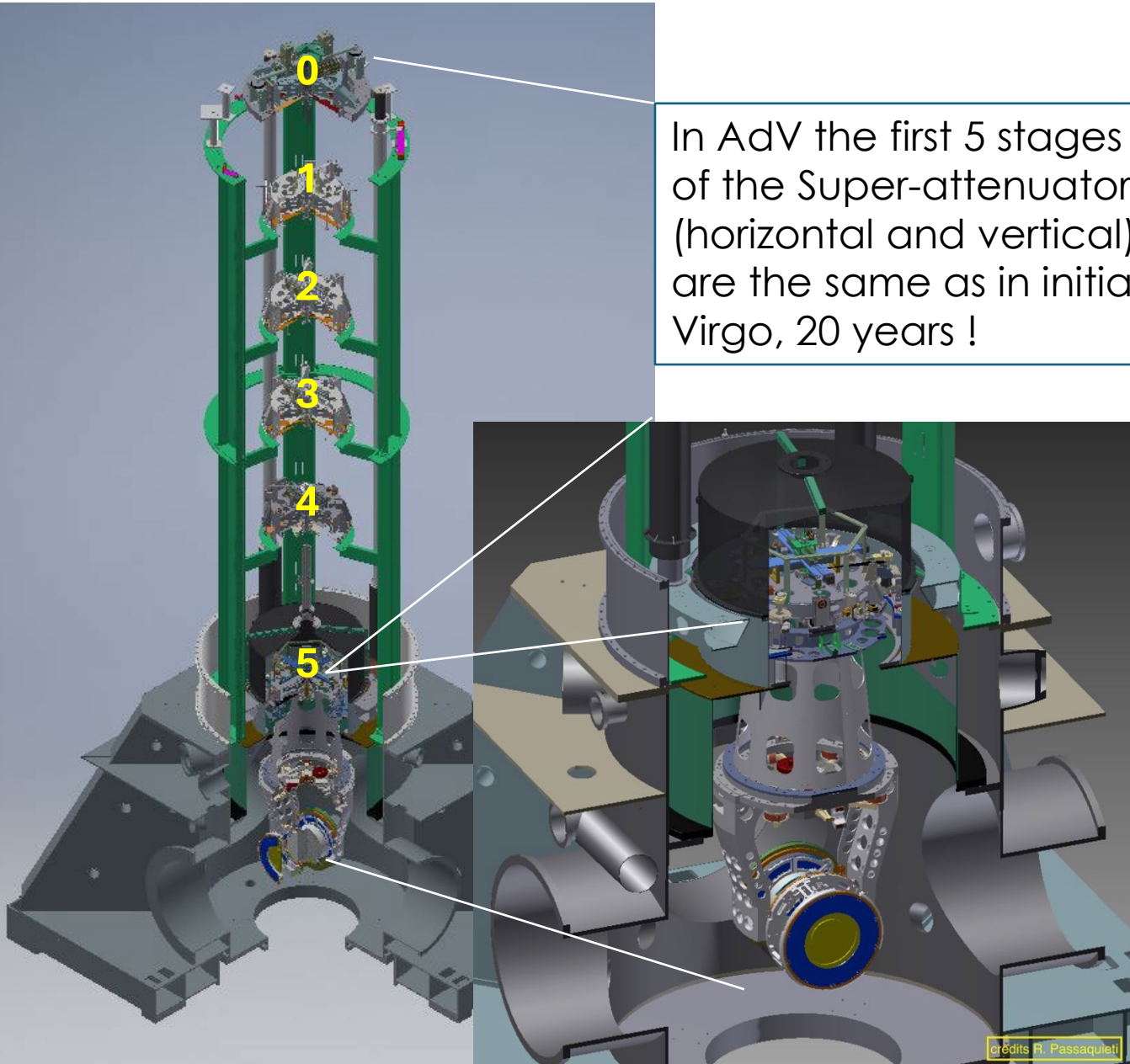
Marionette: Mirror control with actuators (coil-magnets, electrostatic) between the upper suspension stage and marionette

Cage (or Reaction Mass):

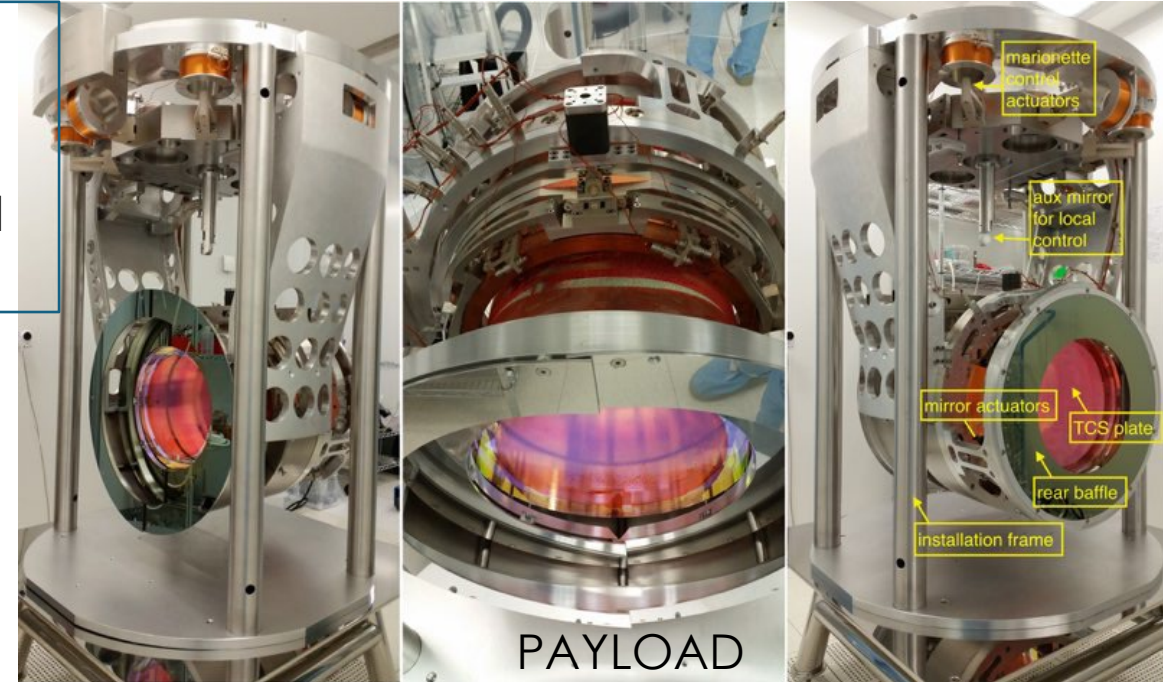
- Test mass and marionette steering with coil-magnets, electrostatic actuation;
- Support for baffle, instrumentation
- Test mass protection

Bernardini A., Majorana E., Puppo P., Rapagnani P., Ricci F., Testi G. "Suspension last stages for the mirrors of the Virgo interferometric gravitational wave antenna." *Rev. Sci. Instr.* 70, no. 8 (1999): 3463.

Test mass suspensions and seismic isolator in AdVirgo: overall system

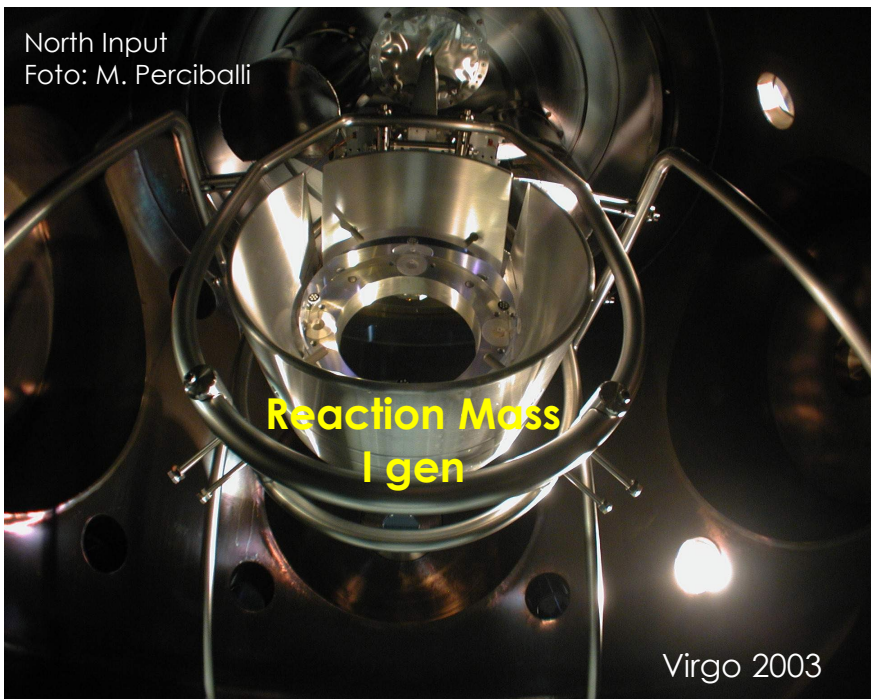


In AdV the first 5 stages of the Super-attenuator (horizontal and vertical) are the same as in initial Virgo, 20 years !

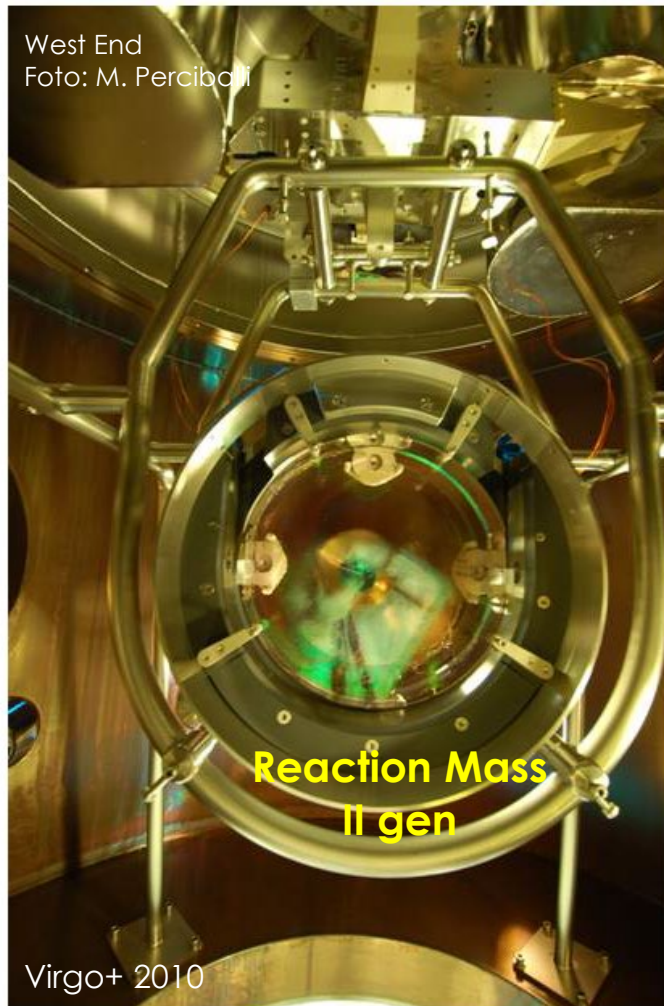


The last filter of the Super-attenuator, prolonged downwards, is in the same vacuum environment of the payload and surrounds it: the “actuation cage”.

Payload evolution in time
Virgo (2003) → AdV (2017)



Masses
20 kg
350 mm diameter – 100 thick
Steel Suspension
with reaction mass



Masses
20 kg
350 mm diameter – 100 thick
Monolithic Suspension
with reaction mass - new



Masses
40 kg mass
350mm diameter – 200 mm thick
Monolithic suspension
with cage

Position Control of test mass

Scheme Last filter + Payload : Virgo → AdV

Virgo

Two Reaction Bodies:

- Physical pendulum for the marionette (F7+Coil Legs)
- Pendulum for the mirror (Reaction Mass)

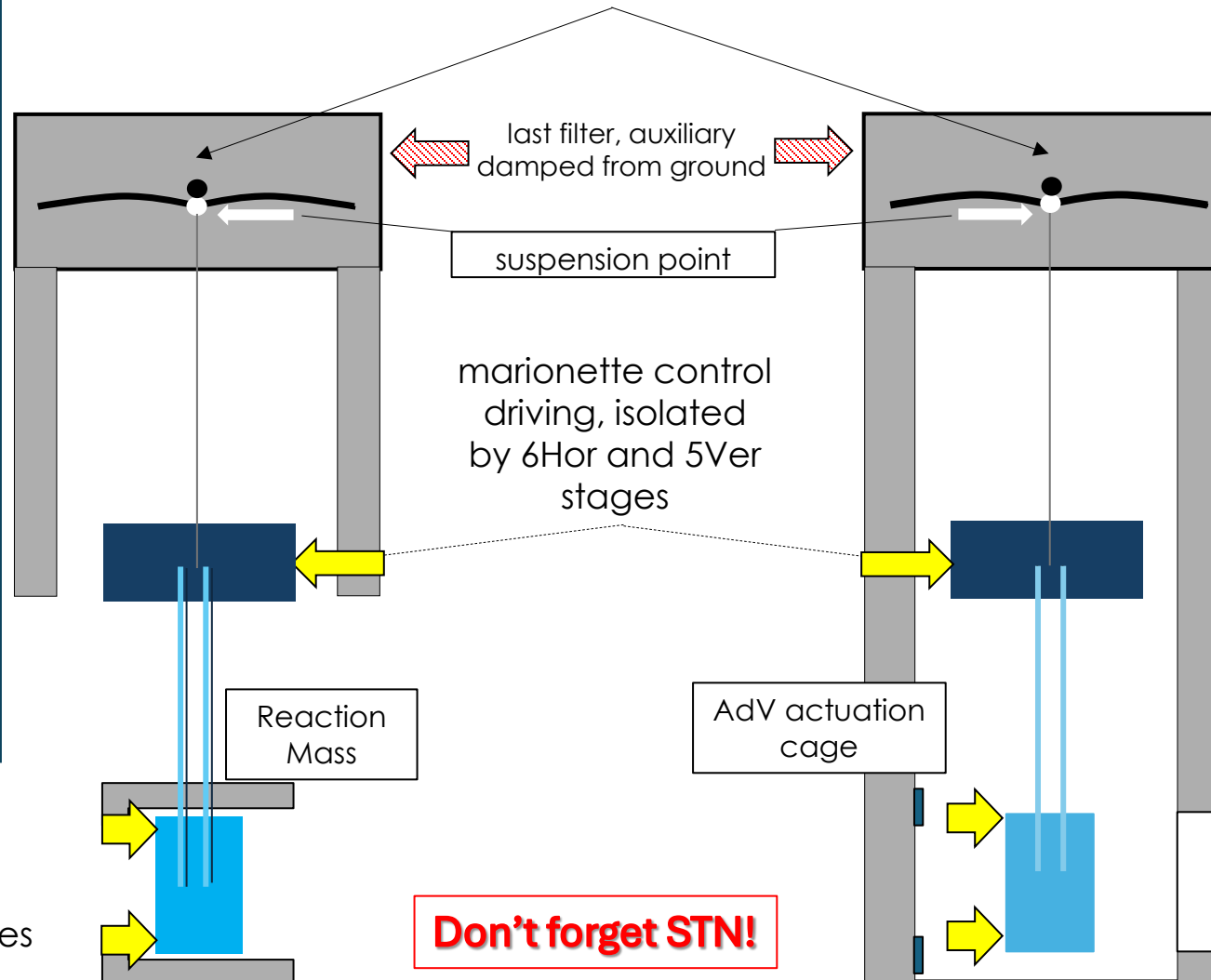
Notice:

- Locking using just actuation on mirror, simple
- hierarchical control (noise minimization) more complex

The TM suspension is a Branched triple pendulum

mirror control driving, isolated by 8Hor and 6Ver stages

5th filter of seismic isolator (F7)



AdVirgo

One Reaction Body

- Physical pendulum (cage) for the simple double pendulum

Notice:

- Locking simple,
- hierarchical control easy

The TM suspension is Double pendulum

mirror control driving, isolated by 6Hor and 5Ver stages

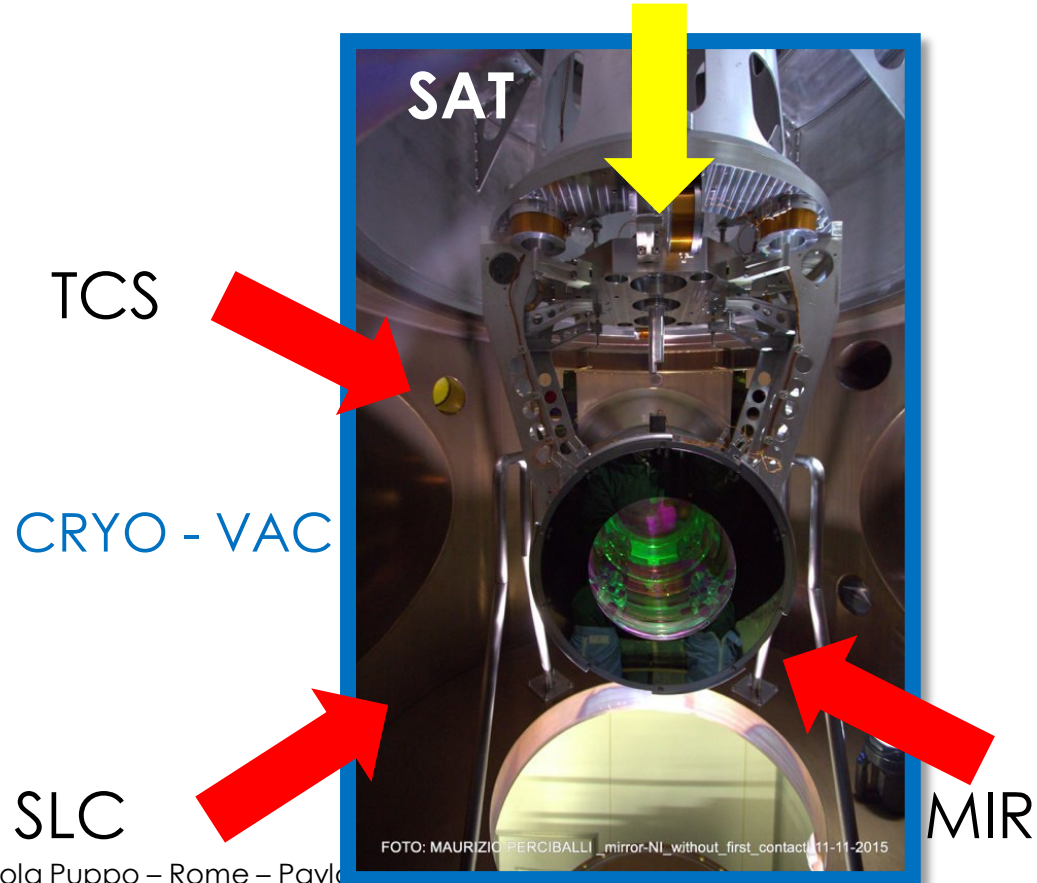
Don't forget STN!



Requirements for the ET Payload

Payloads

- provide the last stage test-mass **suspension controllability** and accomplish with the **mechanical Thermal Noise** requirements;
- is a **composite SubSystem**, strongly interfaced with other SS, in some cases hosting parts of them
- For ET-LF: provide an efficient **heat extraction** from the test-mass to the cryogenic sink (cooling system);



Requirements

- Thermal noise limit
- Materials with low losses and good thermal properties
- Frequencies outside control band and sensitivity band

LF and HF

- Design compliant with the :
 - TM weight
 - Thermal Compensation System TCS (only for HF)
 - Baffles (SLC)

LF Cold

- Heat links connection (low vibrations)
- Thermal Properties, heat inputs, compliance with low cooling time
- Cryostat environment: assembly issues

Important Parameters for the
suspension of the test masses

The bending point

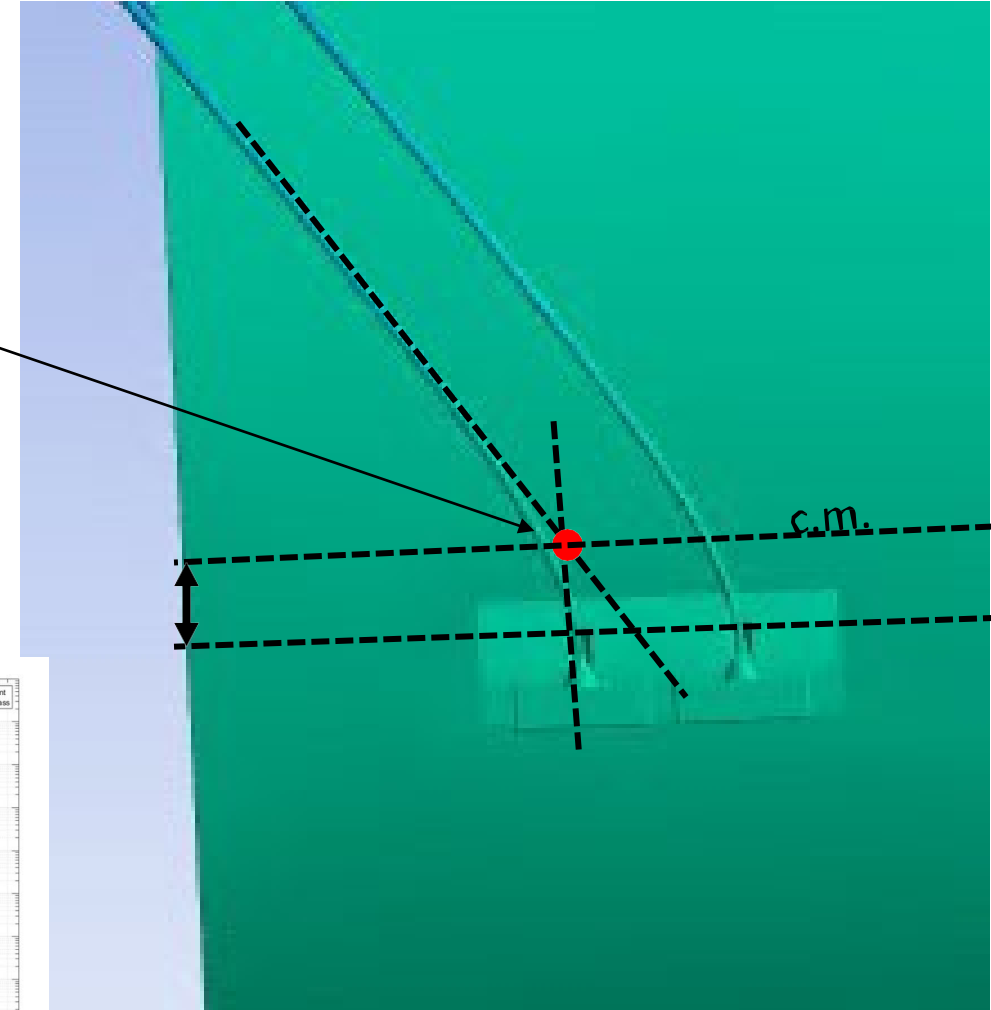
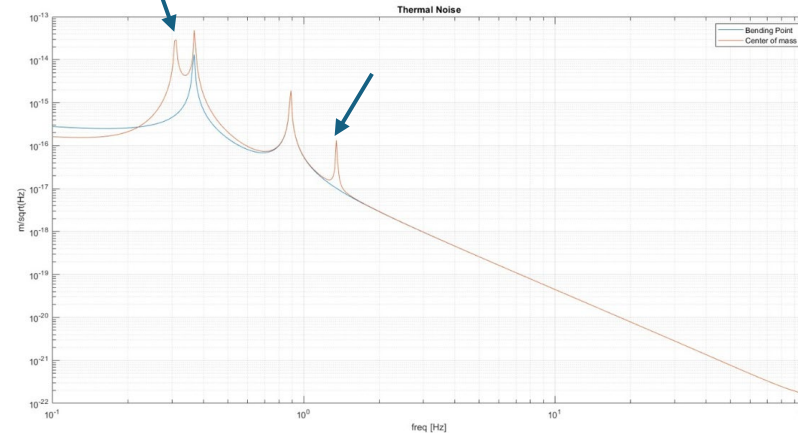
$$\lambda = \sqrt{\frac{Y I}{Tens}}$$

E: Young Modulus
I: Section moment of inertia
Tens: wire tension

The bending point must lay on the center of mass of the suspended body → wire length

$L = L_{cm} + 2\lambda$ for mirrors

Extra peaks due to the wrong susp point → mixed dofs



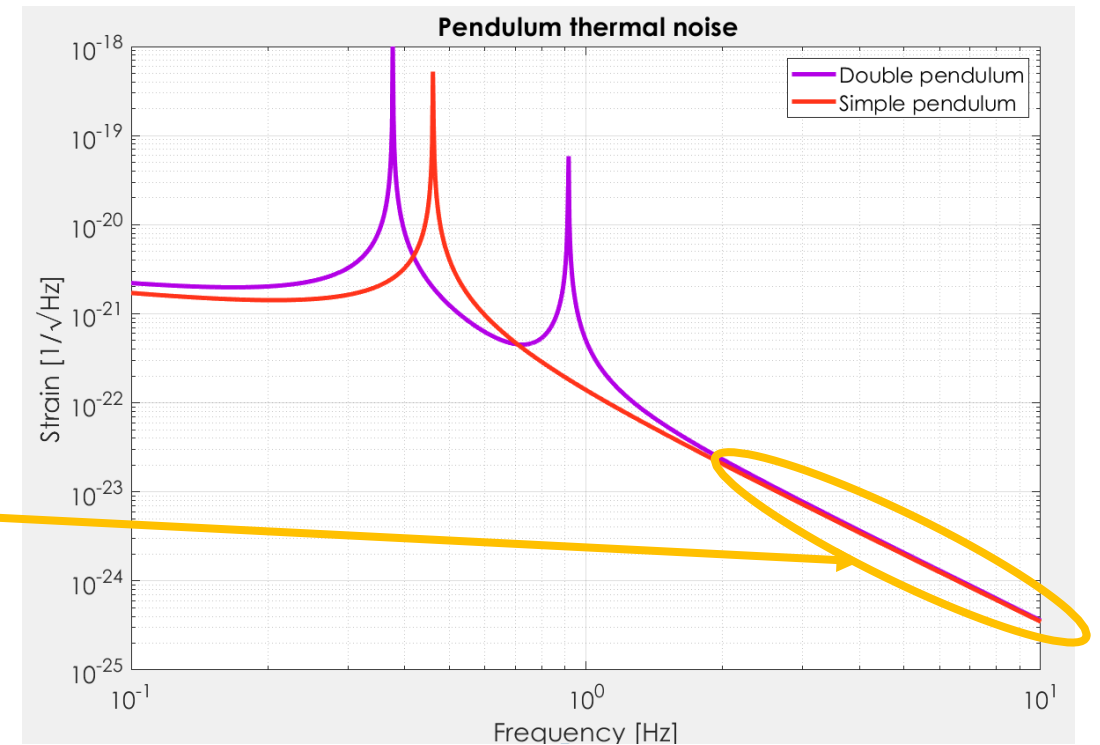
The dilution factor

$$D = \frac{L_w}{2\lambda}$$

E: Young Modulus
I: Section moment of inertia
 L_w : wire length

$$X_{STN}^2(\omega) = \frac{4 k_b T \omega_p^2 \phi_w}{M \omega^5 D}$$

for $\omega \gg \omega_p$



Larger dilution implies a lower level of noise

Heat extraction

Mirror mass 220 kg

Beam size 9cm

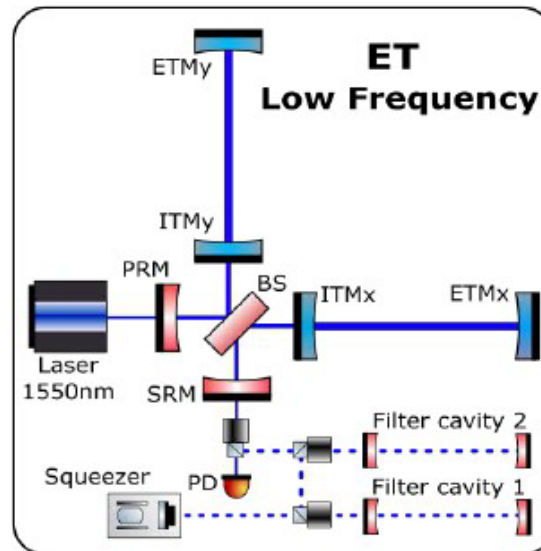
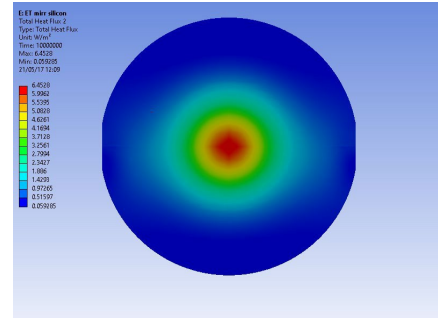
P in the arms 18 kW

Finesse 880

Recycling factor 21.6

$P_{RC}=18\text{kW}/(2F/\pi)=32\text{ W}$ (Power in recycling cavity)

	Sapphire Mirror	Silicon Mirror
Thickness (cm)	35 (diam 450mm)	36 (diam 550mm)
Substrate (ppm/cm)	50	10
Coating (ppm)	1	1
Pcoat (mW)	18	18
Psubstrate (mW)	112	12
Ptot (on ITMs)	130	30
Ptot (on ETMs)	18	18



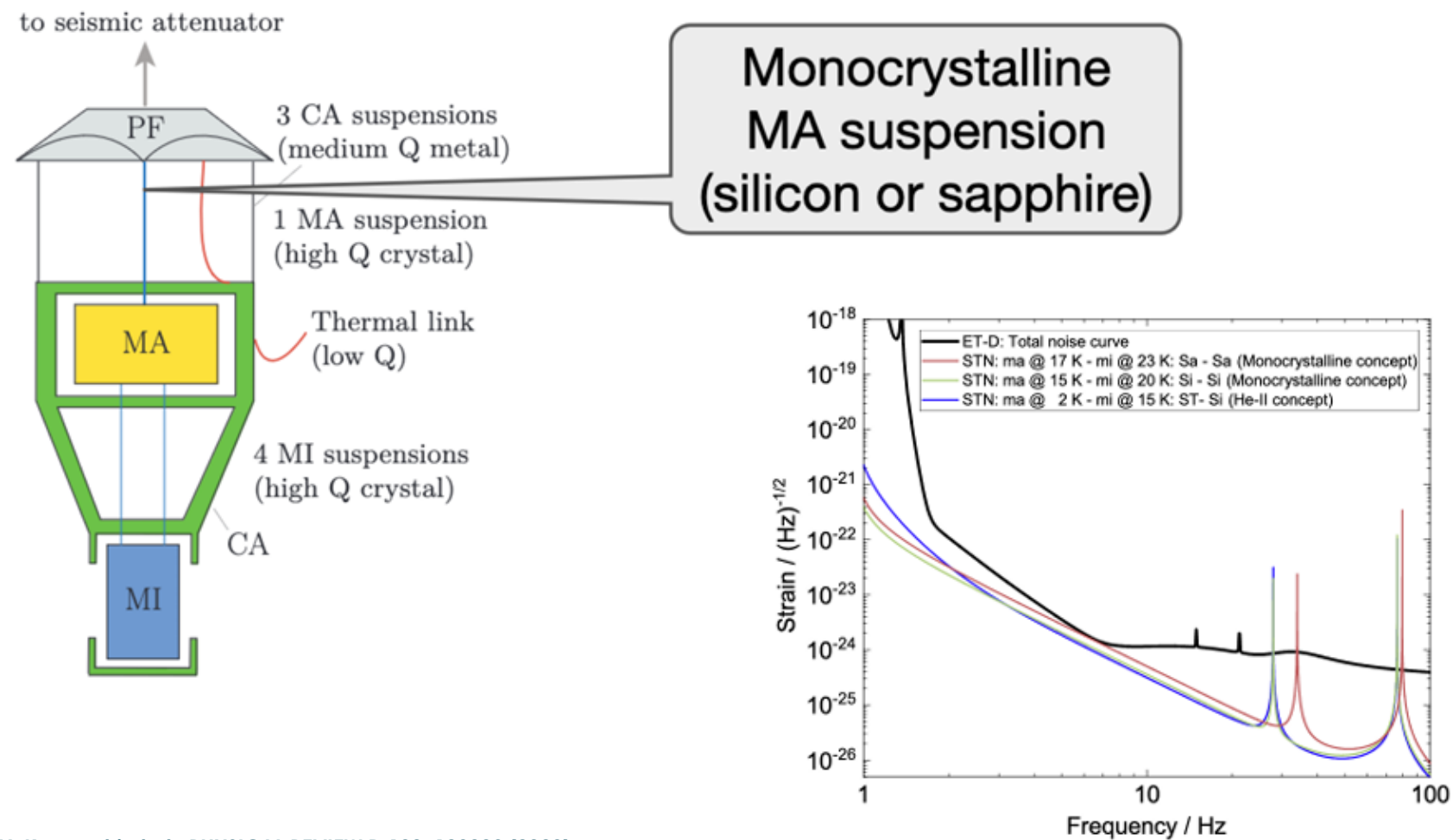
A conservative heat value of **500 mW** is used for the payload design (see M. Ricci presentation).

These aspects have a strong impact on the choice of the cryostat dimensions)

Close integration between suspension and cryogenics necessary

ET-LF payload cooling solutions

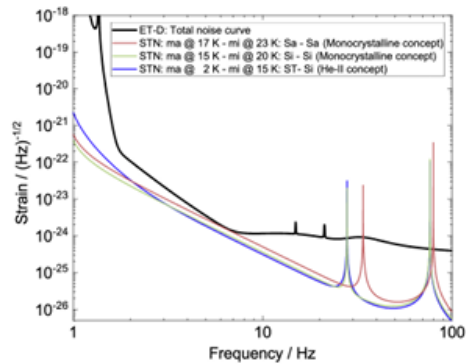
The robust solution → R&D in Roma Sapienza...



	Silicon	Sapphire
Mirror and Marionette Mass (kg)	200	220
Mirror thickness(mm)	360 (diam 550m m)	350 (dia m 450 mm)
Mirror wire - diameter (mm) - length (m)	3.0 1.2	2.3 1.2
Marionetta wire - diameter (mm) - length (m)	8.4 1.0	6.4 1.0
Losses	10 ⁻⁹	5.6 10 ⁻⁹
Temperature (K)	20	20
Wire Tension (Mpa)	77	130
BreakingStrength (Mpa)	200	400

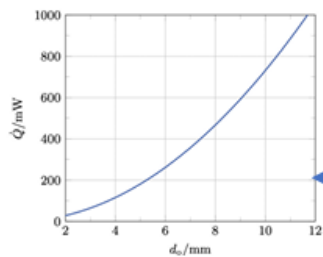
ET-LF payload cooling solutions

Quantum fluid payload → R&D at Karlsruhe Inst. Tech. - KIT

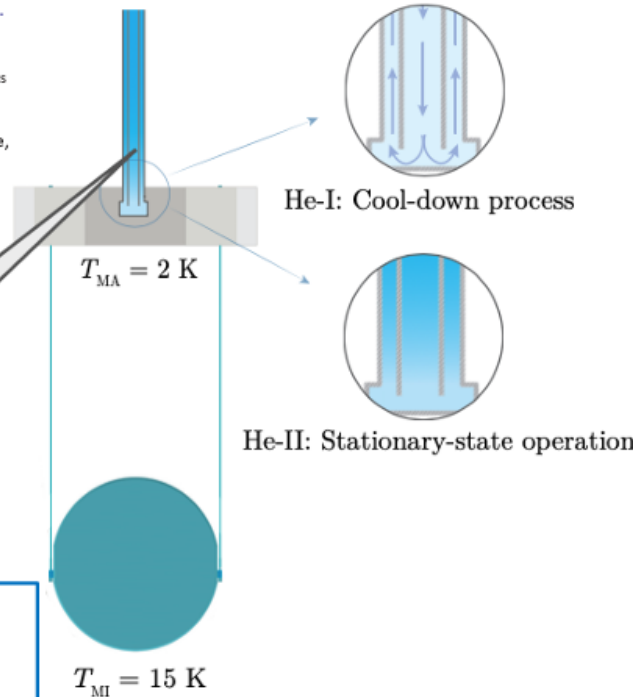


- L. Landau, Theory of the superfluidity of helium II, *Phys. Rev.* 60, 356 (1941).
- S. W. Van Sciver, Helium Cryogenics, 2nd ed., International Cryogenics Monograph Series (Springer, New York, NY, 2012)
- P. Puppo and F. Ricci, Cryogenics and Einstein telescope, *Gen. Relativ. Gravit.* 43, 657 (2011)
- X. Korovesi et al. Physical Review D 108.123009

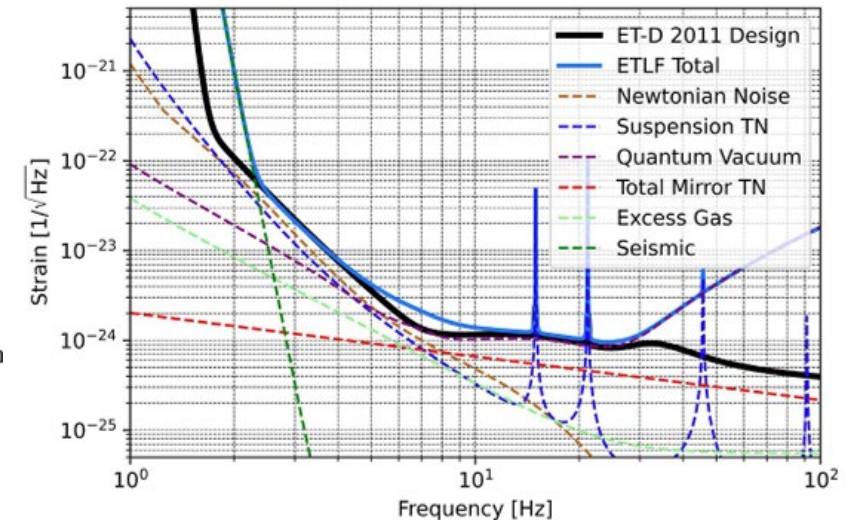
He-II filled MA suspension tube (titanium)



Cooling capacity of the He-II suspension as function of the outer tube diameter.



Cryogenic ET-LF



X. Korovesi, S. Grohmann, P. Rapagnani, and V. Mangano, Experimental plans to validate the He-II based payload cooling concept, ECLoud and GWDVac'22 Workshops, Portoferraio, Italy (2022), [10.5445/IR/1000153742/v2](https://arxiv.org/abs/10.5445/IR/1000153742/v2).

Design of the payload (recursive)

Mechanical design

- Materials → Mechanical, thermal properties, losses
- Breaking strength
- Interfaces → HCB, couplings
- Shapes of wires (diameter, length)
- Frequencies:
 - Must be outside sensitivity bandwidth
 - Must be compliant with control requirements
- Seismic attenuator interface

Thermal design (for Cryo-Pay)

Cooling efficiency, cryostat design, Heat to be extracted

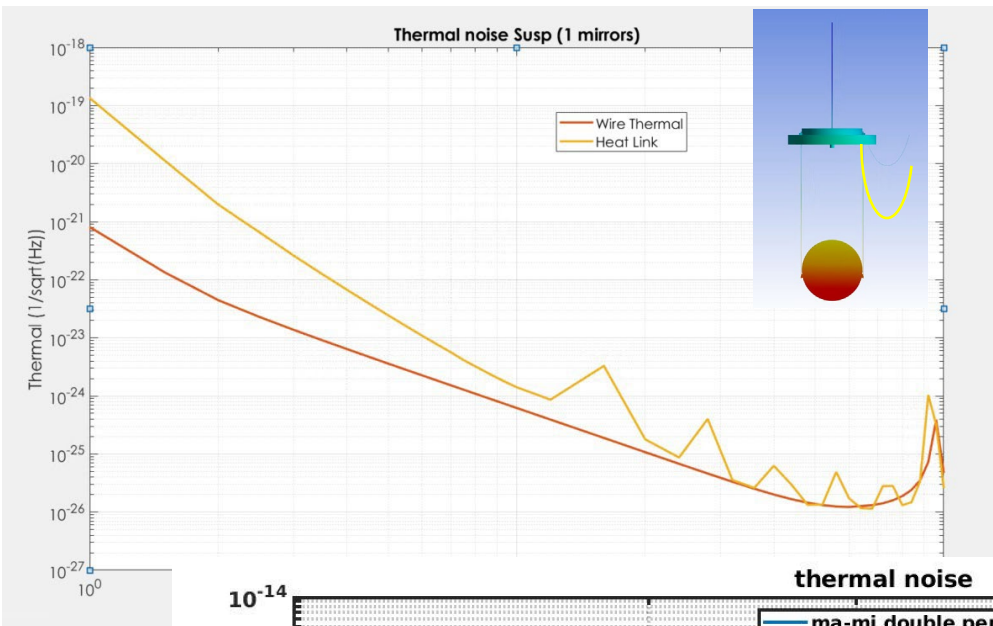
- Heat extraction
 - No noise injection from links
 - Thermal resistance of the interfaces as low as possible

Suspension Thermal noise → Sensitivity

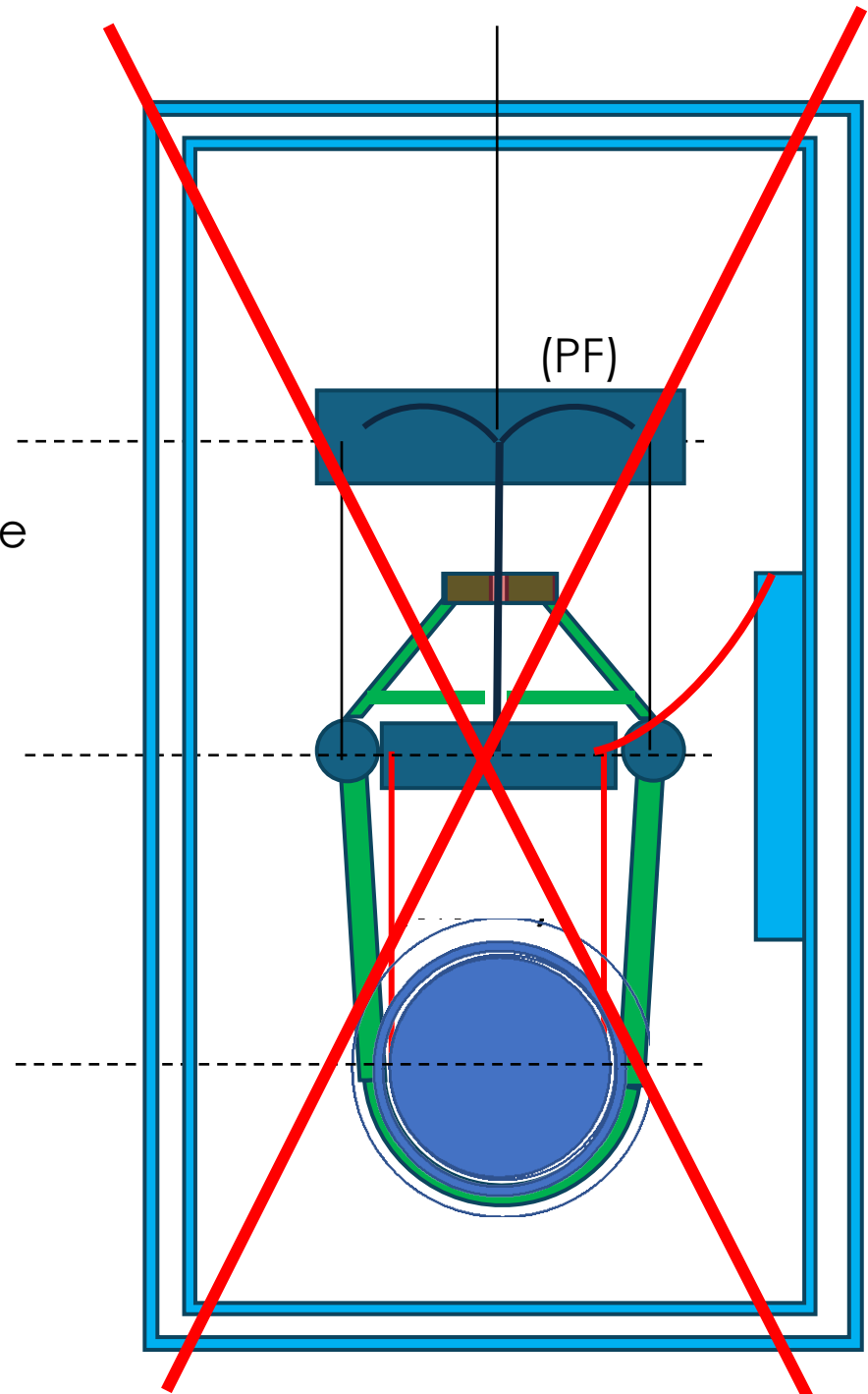
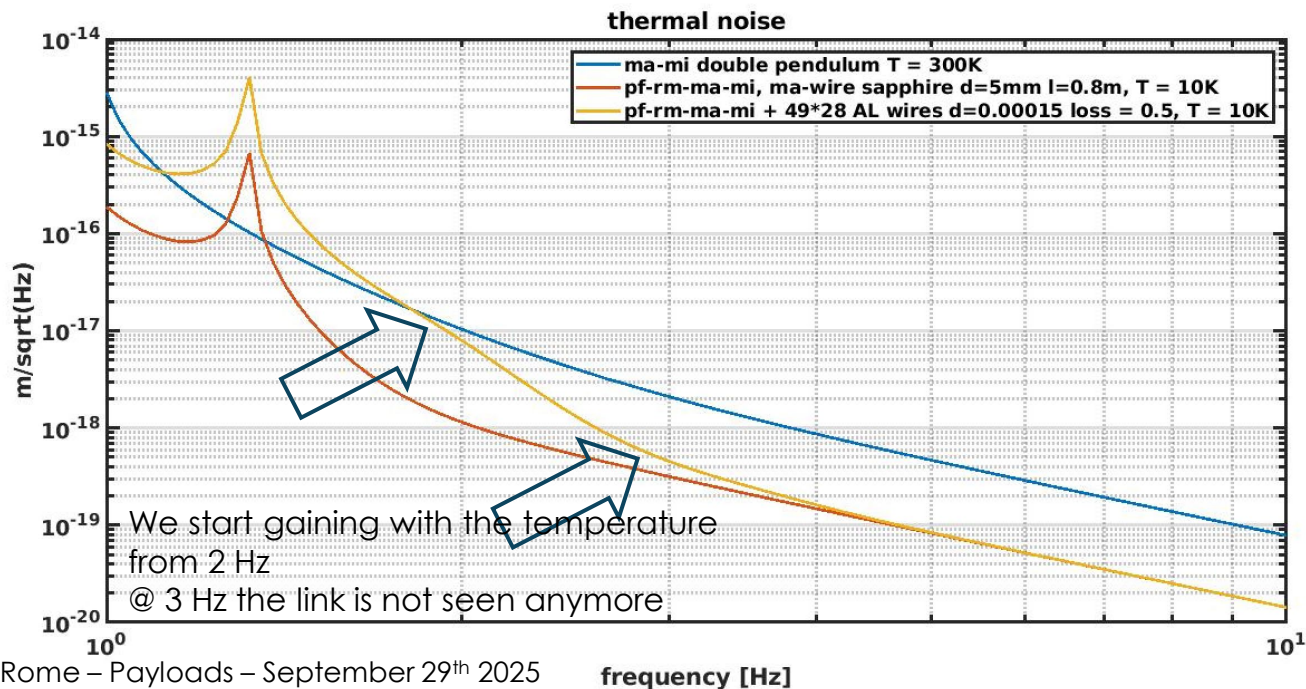
Noise limit : $3 \cdot 10^{-20} \text{ m/sqrt(Hz)}$, $5 \cdot 10^{-21} \text{ m/sqrt(Hz)}$ @ 10 Hz

Issue on heat links (see also M. Ricci presentation)

Pure Aluminum Heat Link (loss angle: 0.5)



- The Heat Links cannot be directly connected to the marionette, they introduce vibrations and also increase the STN



The vertical noise issue

$$STN_{total} = STN_{hor} + g_{coupling}^2 STN_{ver}$$

↑
pendulum

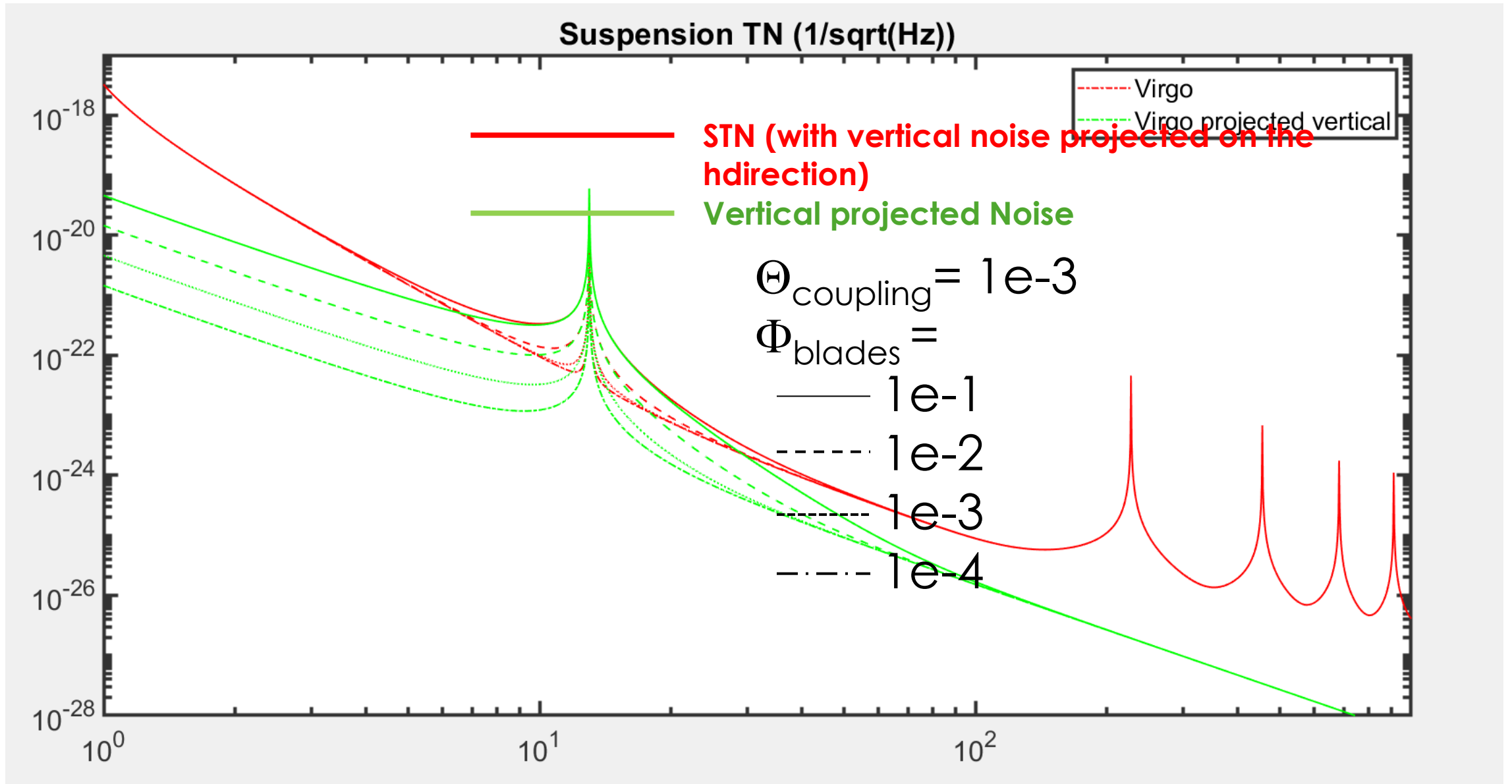
$$STN_{hor}(\omega) = \frac{4k_b T}{m \omega} \cdot \frac{\omega_p^2 \Phi_p(\omega)}{\left((\omega_p^2 - \omega^2)^2 + (\omega_p^2 \Phi_p(\omega))^2 \right)}$$

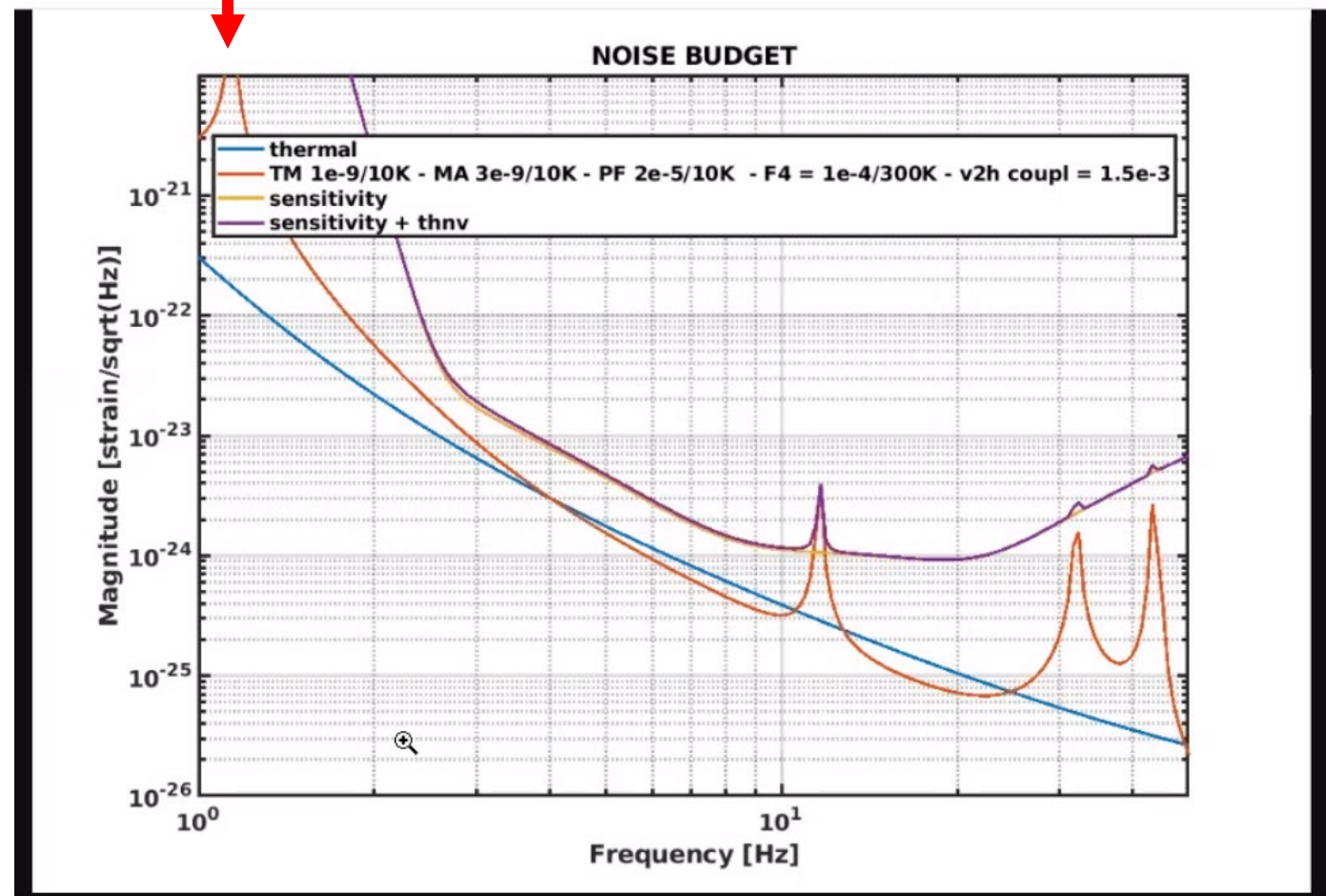
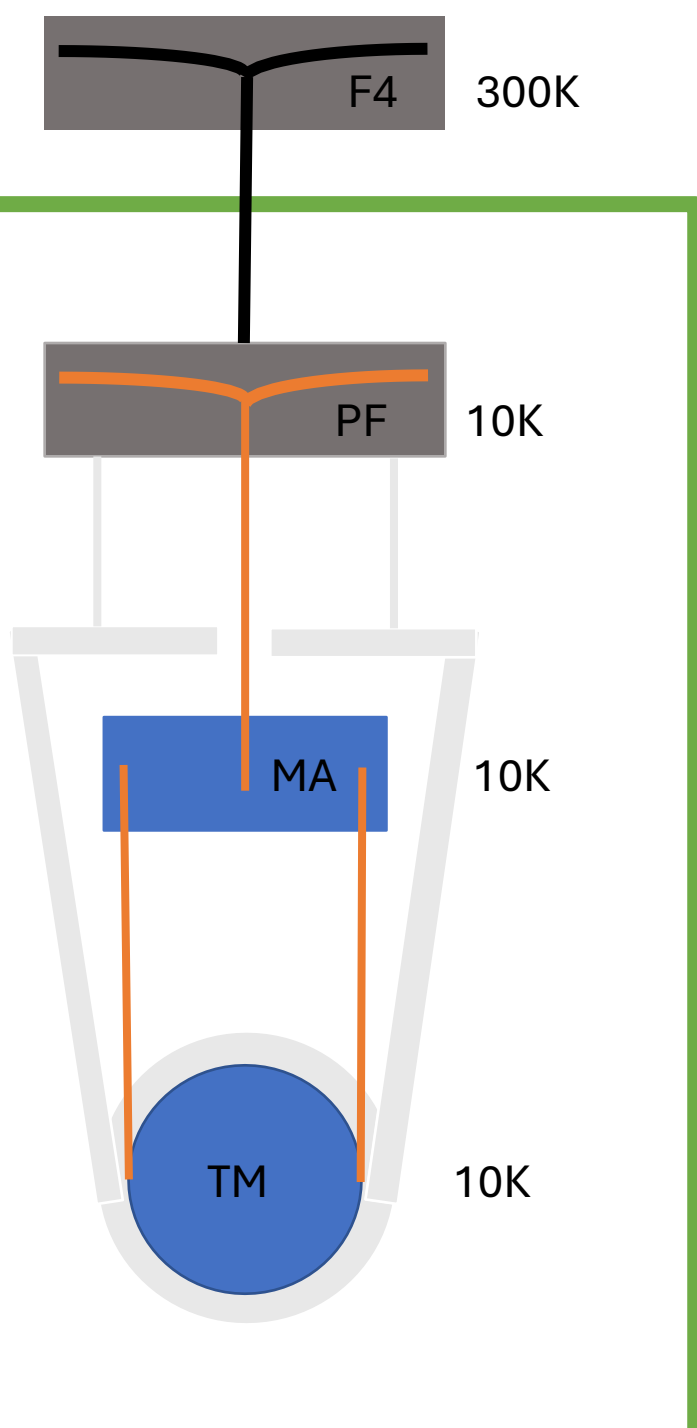
$$STN_{ver}(\omega) = \frac{4k_b T}{m \omega} \cdot \frac{\omega_{ver}^2 \Phi(\omega)}{\left((\omega_{ver}^2 - \omega^2)^2 + (\omega_{ver}^2 \Phi(\omega))^2 \right)}$$

The loss angle of the pendulum is the loss angle of the wire material diluted by the presence of gravity.

The loss angle in the vertical is not diluted

Virgo STN





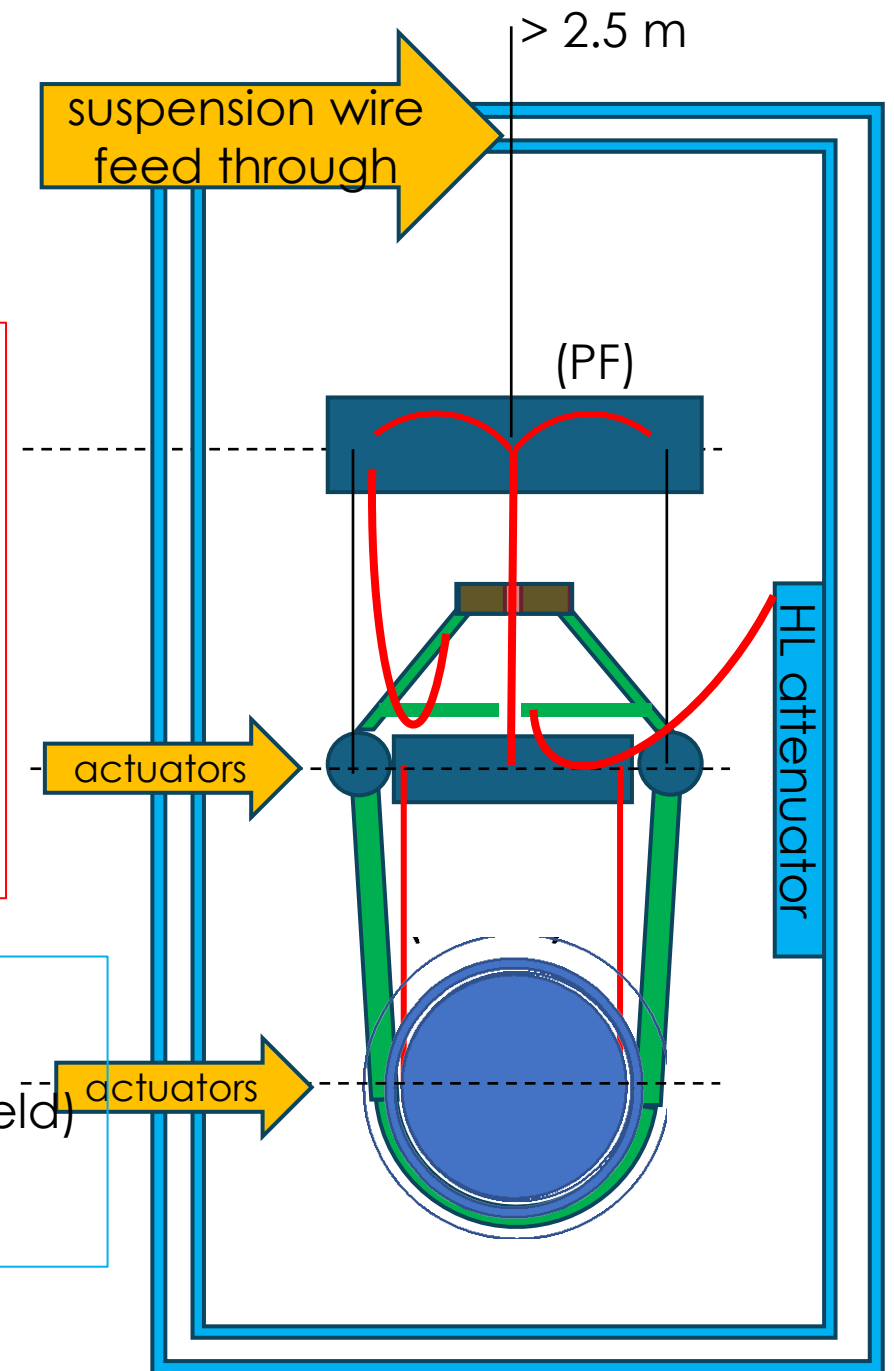
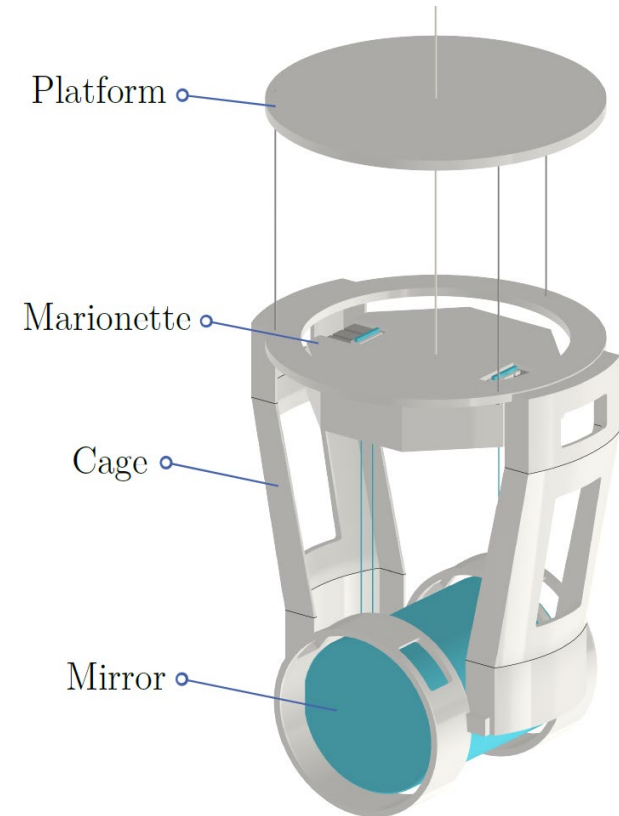
Paolo Ruggi computation of VTN (orange) with Octopus

Cooling and LF Payload parameters

- Heat path the cage – platform – test mass
- Heat link attenuated

- Mirror Mass = M
- Cage(RM) = M
COM (center of mass) on PF COM
- Marionette = M
- PF Mass = $M+M/2$
- **Large mirrors (max diam 600mm)**
- Interval in the PBS is 140-220 kg
- On F7 = $M = 0.7-0.9$ Tons
- **Lmir (0.7-2)m**
- **Lmario (0.7-2)m**
- **LPF>2.5m**

Dimensions of the cryostat
 Max diam = 3 m
 Max Height = 3.8 m (innermost Cryo Shield)
 Preferred the insertion from bottom side



Cold Payload (ET-LF) Activities & Projects

ETIC ARC Cryo and LoVeC-ET projects at Rome University

- Payload prototype. Virgo-like. Material sapphire
- Cryostat prototype

Project at **KIT** for a superfluid helium suspension cable.

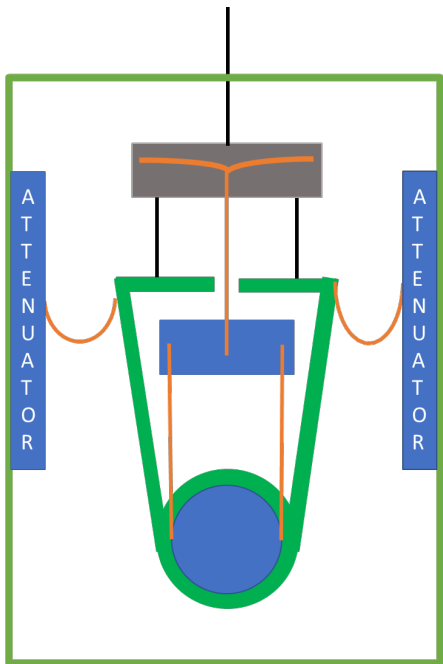
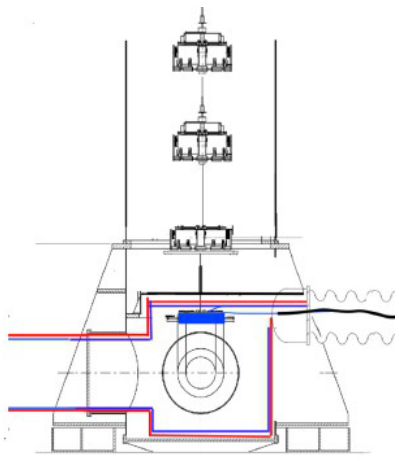
Glasgow: cryo payload on small scale, Ligo-like, silicon mirror suspended with sapphire wires, welding possible. Large scale with PT cooling is foreseen in future for test.

Nikhef: ET-Pathfinder

Other studies: Payload with compressed flexures (De Salvo),...

People involved in the Virgo-like payload:

- **Rome:** A. Cruciani, E. Majorana, V. Mangano, L. Naticchioni, S. Pirro, P. Puppo, P. Rapagnani, F. Ricci, M. Ricci, E. Tofani Eng: E. Benedetti, F. Hoang, M. Orsini, D. Pasciuto.
- **EGO:** P. Ruggi
- **KIT** (Karlsruhe Institute of Technology): S. Grohmann
- **KAGRA collaborators**



Some comments on the overall mass (and TM)

- **Maximum allowed weight change for the Seismic Suspension:** 0.7 – 0.8 Tons (adjustment tolerance on payload - ballast);
- 10 kg per stage adjustment (on SA) without changing the blades;
- **The weight on payload** can be adjusted on ballast on payload;
- The value of TM is taken that as a starting point, as some sub-systems are ready for that.
- **Heat load must be considered** (300 mW on mirror and the rest on the payload (overall 500 mW))
- Heat load due to electrical cabling (considered in recent modelling at KIT) and viewports (in KAGRA the radiation through the viewports has negligible impact)
- TM mass impacts on QN → sensitivity range

Comments and Outlook

- Different concepts for monolithic solutions employing silicon or sapphire are in the panorama for ET-LF;
- Different cooling technologies
(CryoFluids, Pulse Tubes Rome, Quantum Fluid cooling KIT)
- Heat links issues
- Vertical noise issues → study on low loss blades are important
- From M. Pinto talk. Pitch frequency important for angular control and noise → increase dZ (distance between wires)...depends also on mirror material, birefringence...

See the next talks for the mechanical and thermal studies of the Virgo-like cryo-payload (M. Ricci and E. Benedetti)